EFFICIENCY OF OXYGEN-ABSORBING SACHETS IN DIFFERENT RELATIVE HUMIDITIES AND TEMPERATURES

Renato Souza Cruz1, Nilda de Fátima Ferreira Soares2, Nélio José de Andrade3

ABSTRACT

The main objective of this work was to evaluate the efficiency of oxygen-absorbing sachets at relative humidity of 75%, 80% and 85% and different temperatures, 10±2 ºC and 25±2 ºC. The experiment consisted in determining the O2 absorption under these conditions. A sachet was placed in desiccators with an internal air homogenization system. Aliquots of air were removed at pre-established time intervals and analyzed for oxygen content. The results showed that oxygen absorption by the sachet increased as the relative humidity increased for both temperature. Therefore, the oxygen-absorbing sachets were most active under 25±2 ºC and 85% relative humidity. At ambient condition (25±2 ºC/75%RH) the rate of oxygen absorbed was 50 mL/day and 18.5 mL/day for 10±2 ºC. It was used a totally casualized design with three replicates.

Index terms: Active packaging, oxygen-absorbing, relative humidity, temperature.

INTRODUCTION

The presence of oxygen (O2) in packages is mainly due to failures in the packaging process, such as mixture of gases containing oxygen residues, inefficient vacuum as well as high rates of oxygen permeability through the packaging film utilized. Therefore, research and developments in the area of packaging have been conducted, aiming to eliminate residual O2. Within this context, the concept of active packaging was introduced. Such packaging interacts with the packaged product, modifying its properties in a desirable manner (ROONEY, 1995).

This new concept of packaging includes: oxygen and ethylene scavengers, carbon dioxide — scavengers and emitters, humidity and flavor controllers, films incorporated with antimicrobial and anti oxidant agents or displaying biodegradable properties (BERENZON & SAGUY, 1998; HAN, 2002; VERMEIREN et al., 1999).

Overall, oxygen absorbing technology is based on oxidation or combination of one of the following components: iron powder, ascorbic acid, photosensitive polymers, enzymes, etc (FLOROS et al., 1997; LABUZA & BREENE, 1989; ROONEY, 1995; VERMEIREN et al., 1999). These compounds are packaged into permeable material, usually in the form of sachets (ABE & KONDOH, 1989; NAKAMURA & HOSHINO, 1983). According to Abbott (2002) the main advantages in using absorbers are their ability to reduce the levels of oxygen to below 0.01%, which is lower than the levels typically found (0.3-3%) in the conventional systems of modified atmosphere, vacuum or substitution of internal atmosphere for inert gas. Thus, this method has attracted
attention as a new packaging technology to preserve food that needs reduced levels of oxygen inside the packages (ABE & KONDOH, 1989; NAKAMURA & HOSHINO, 1983).

In order to obtain a greater absorbing effectiveness, some conditions must be met, such as, using containers or films providing a high oxygen barrier (oxygen-permeability rate of up to 20 cm$^3$/m$^2$.atm.day), films or recipients with good sealability. Another important parameter is selecting the appropriate absorber, i. e., type, size, capacity (NAKAMURA & HOSHINO, 1983). Physical state, water activity in the food, the amount of oxygen dissolved in the product and the initial level of oxygen in package read space also must be taken into consideration (SMITH et al., 1990, 1995). When using absorbers in the form of sachets, a free air flow around the sachet is also needed, in order to enhance the oxygen-scavenging efficiency in the package (AZEREDO et al., 2000; SMITH et al., 1990, 1995). All these factors will contribute to the oxygen absorbers efficiency so that reduction of the oxygen level in the package could occur in a minimum time.

This work aimed to evaluate the absorption efficiency of a commercial oxygen absorbing system in the presence of different relative humidity levels, 75%, 80% and 85% and at 10±ºC and 25±ºC.

MATERIAL AND METHODS

The absorbing system used was sachet containing iron-based compounds O-Buster brand, FT-300 model, develop to be used in products with maximum water activity (Aw) of 0.85. The absorption capacity of the sachet, according to the manufacturer, is of up to 300 mL of oxygen. The experiment was realized in entirely randomized design with three replicates.

Determination of the absorption curve of sachets under different levels of relative humidity and temperatures

The system used in the experiment consisted of 5.5 L capacity desiccators, each containing one absorbing sachet. The desiccator lids contained silicone septa through which air samples were taken and analyzed by oxygen analyzer (MOCON). A ventilation system was installed inside each desiccator, so that the air could be homogenized before being collected for analysis. The system was maintained hermetically sealed.

Relative humidity of 75, 80 and 85% inside the desiccators was obtained, by using saturated solutions of sodium chloride, ammonium sulfate and potassium chloride, specific each one. Aliquots of 3 mL were collected for the experiment conducted at 25±2ºC every 30 minutes, up to the first four hours and every four hours, afterwards. For the experiment under temperature of 25±2ºC, the intervals were every hour during the first 12 hours and every 12 hours, afterwards. Under both temperatures, the samples were collected until no oxygen absorption by the sachet was confirmed.

RESULTS AND DISCUSSION

Effect of relative humidity and temperature on the rate of oxygen absorption by use of sachets

Oxygen absorption by use of sachets is dependent on environmental factors, such as relative humidity and temperature. The results shown that the greater the relative humidity, the greater and faster the oxygen absorption by the sachet, for both storage temperatures. This fact is due to the need of the presence of water for the reaction between the oxygen molecule and the iron to occur. (Figures 1 and 2).
The effect of relative humidity on the oxygen-iron reaction may be observed in the variation of activation energy (Ae) shown in Table 1, calculated by the Arrhenius equation (Eq 1).

\[
\frac{-Ae}{K} = K_0 * e^{RT},
\]

Arrhenius equation, which through mathematical transformation, can be thus written:

\[
\ln(K) = -\frac{Ae}{R} \left(\frac{1}{T}\right) + c
\]

where

- \( Ae \) - Activation energy
- \( R \) - Constant of gases, 8,314 J/mol.K
- \( T \) - Absolute temperature, Kelvin degree
- \( K \) - Sachet absorption rate

Table 1 – Activation energy resulting from the iron-oxygen reaction for the different rates of relative humidity and temperature variation from 10±2°C to 25±2°C.

<table>
<thead>
<tr>
<th>Relative humidity (%)</th>
<th>Ae (KJ/mol)</th>
</tr>
</thead>
<tbody>
<tr>
<td>75</td>
<td>60.53±1.53ª</td>
</tr>
<tr>
<td>80</td>
<td>60.09±1.14ª</td>
</tr>
<tr>
<td>85</td>
<td>55.91±0.71b</td>
</tr>
</tbody>
</table>

Means followed by same letters do not differ significantly by the Tukey test (p<0.05).

The highest sachet absorption rate was found for relative humidity of 85%, which, under this condition, presents lower activation energy, whose value was 55.91±0.71 KJ/mol (Table 1).

Temperature was also found to influence the rate of oxygen absorption by use of sachets. It should be emphasized that in both experiments, the amounts of oxygen absorbed, 420 mL and 570 mL, for temperatures 10±2°C and 25±2°C, respectively, were higher than 300 mL, the amount indicated by the manufacturer. This value was reached for the experiment at 10±2°C around day 6 for humidity of 80 and 85%, and around day 10 for humidity of 75%. For the experiment at 25±2°C, the amount indicated by the manufacturer was obtained after 24 hours for 80 and 85% of relative humidity and, around 36 hours for 75% of relative humidity.

The maximum amount of oxygen absorbed by use of sachet for the experiment at 10±2°C was lower than for the experiment at 25±2°C for all the relative humidity rates studied (Table 2). This can be explained by the fact that the absorbing system utilized absorbs oxygen through a chemical reaction, thereby being influenced by temperature, where at higher temperatures, the velocity of reaction is higher.

Table 2 – Maximum amount absorbed by use of sachet at different temperatures and relative humidity rates.

<table>
<thead>
<tr>
<th>Relative humidity (%)</th>
<th>Maximum amount absorbed</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>10±2°C</td>
</tr>
<tr>
<td>75</td>
<td>363.13 ± 8.72</td>
</tr>
<tr>
<td>80</td>
<td>424.65 ± 3.25</td>
</tr>
<tr>
<td>85</td>
<td>474.96 ± 1.8</td>
</tr>
</tbody>
</table>

The volume of oxygen absorbed by the sachet decreases asymptotically along time, due to the irreversible reaction of iron to oxygen, which is available in excess (Figure 3 and 4). Another fact is the formation of a barrier by the ferrous particles nearest to the sachet walls that, when reacting, form a stable compound, iron hydroxide, hindering the contact of oxygen with the ferrous particles inside the sachet.

No considerable difference was observed in the absorption rate of the sachets stored at different relative humidity rates for both storage temperatures (Figures 5 and 6). However, such rate was influenced by temperature with values of 50mL/day and 18,5mL/day for temperatures of 25 ±2°C and 10 ±2°C, respectively.
This fact was likely due to the presence of agents such as silica or ascorbic acid (DELDUCA et al., 2001) which are incorporated into the sachet compounds, accelerating the reaction. At the first 12 hours the humidity present in the desiccator is enough to start the reaction. After the different levels of relative humidity are reached, a differentiation in the absorption rates occurs according to the relative humidity rates. Temperature influenced the rate of oxygen absorbed by use of sachet in all the relative humidity values studied. Overall, a decrease of 57% was observed in the absorption rate by use of sachet as temperature decreased from 25±2°C to 10±2°C.

The oxygen-absorbing sachets presented more activity at 25±2°C and 85% of relative humidity. The absorbers tested, FT-300 of O-Buster, showed a greater absorption capacity than that indicated by the manufacturer.

Under the average storage conditions in Brazil (25±2°C and 75% RH), the sachets presented absorption of approximately 500mL of oxygen. At a temperature of 10±2°C and 75% RH there was a reduction of 28%, and a maximum of O₂ absorption of approximately 360mL.

**CONCLUSION**

The oxygen-absorbing sachets presented more activity at 25±2°C and 85% of relative humidity, absorbing 650 mL of oxygen. When the typical Brazilian condition 25±2°C e 75% RH presented absorption of approximately 500mL of oxygen. In both cases, the amount absorbed by the sachet was higher than the manufacturer recommendation - 300 mL. Therefore, the oxygen-absorbing sachets is an efficient device to remove oxygen from the interior of the packaging.

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